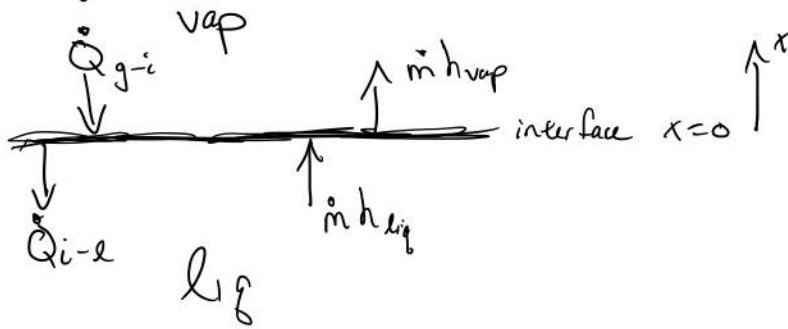


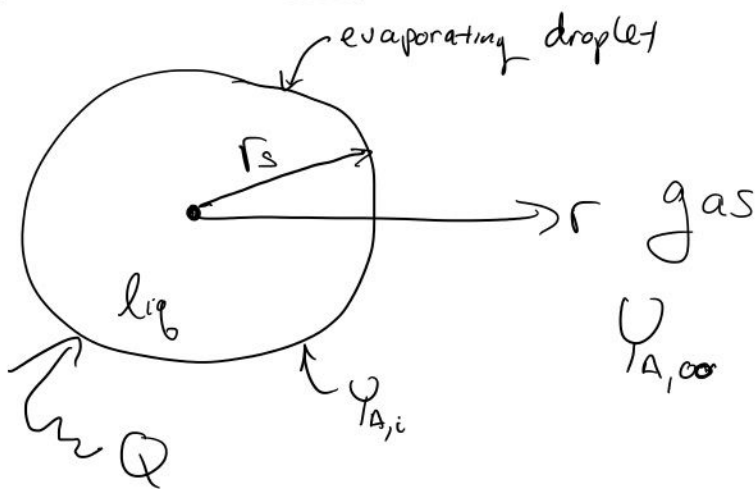
$$T_{\text{liq},i}(x=0^-) = T_{\text{vap},i}(x=0^+) = T(0)$$



energy balance: $\dot{Q}_{g-i} - \dot{Q}_{i-e} = \dot{m}(h_{\text{vap}} - h_{\text{liq}})$

$$\dot{Q}_{\text{net}} = \dot{m} h_{\text{fg}}$$

Droplet Evaporation



- radius is our only coordinate variable (r)
- r_s changes w/ time
- $r \rightarrow \infty \quad y_A = y_{A,\infty}$
- heat from ambient gas supplies the

- heat for evaporation"
- ignore chemistry

eqn for system:

- mass cons. for droplet
- mass cons. for surroundings
- energy cons. for droplet
- energy cons. for surroundings
- mass cons. across the boundary

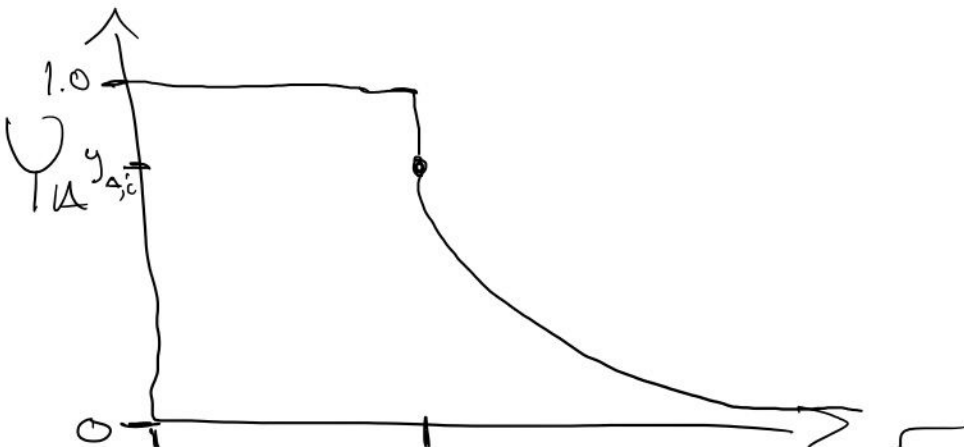
Assumptions:

#1: Quasi-steady state evaporation

#2: Droplet T is uniform

#3: $x_{A,i} = \frac{p_{\text{sat}}(T_{d,i})}{p}$ (vapor-liq. equil.)

#4: thermo physical properties are constant



- heat for evaporation"
- ignore chemistry

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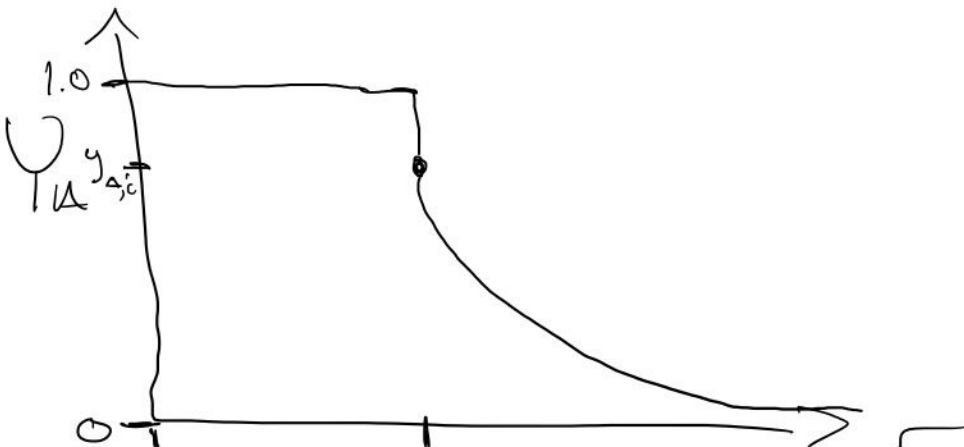
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#1: Quasi-steady state evaporation

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#3: $x_{A,i} = \frac{p_{\text{sat}}(T_{d,i})}{p}$ (vapor-liq. equil.)

#4: thermo physical properties are constant



Apply BC $r=r_s$, $Y_A = Y_{A,s}$

$$\ln(1 - Y_{A,s}) + \frac{\dot{m}}{4\pi r_s \rho D_{AB}} = C$$

$$\Rightarrow \frac{\dot{m}}{4\pi r \rho D_{AB}} = -\ln(1 - Y_A) + \ln(1 - Y_{A,s}) + \frac{\dot{m}}{4\pi r_s \rho D_{AB}}$$

$$-\frac{\dot{m}}{4\pi \rho D_{AB}} \left(\frac{1}{r_s} - \frac{1}{r} \right) = \ln \left(\frac{1 - Y_{A,s}}{1 - Y_A} \right)$$

$$\frac{\exp\left(\frac{-\dot{m}}{4\pi \rho D_{AB} r_s}\right)}{\exp\left(\frac{-\dot{m}}{4\pi \rho D_{AB} r}\right)} = \frac{1 - Y_{A,s}}{1 - Y_A}$$

$$\Rightarrow Y_A(r) = 1 - (1 - Y_{A,s}) \frac{\exp\left(\frac{-\dot{m}}{4\pi \rho D_{AB} r}\right)}{\exp\left(\frac{-\dot{m}}{4\pi \rho D_{AB} r_s}\right)}$$

Apply BC $\rightarrow r \rightarrow \infty$ $Y_A \rightarrow Y_{A,\infty}$

$$Y_{A,\infty} = 1 - (1 - Y_{A,s}) \frac{\exp\left(\frac{-\dot{m}}{4\pi \rho D_{AB} \infty}\right)}{\exp\left(\frac{-\dot{m}}{4\pi \rho D_{AB} r_s}\right)}$$

$$\frac{(1 - Y_{A,\infty})}{(1 - Y_{A,s})} = \exp\left(\frac{-\dot{m}}{4\pi \rho D_{AB} r_s}\right)$$

$$\dot{m} = 4\pi \rho D_{AB} r_s \ln \left(\frac{1 - Y_{A,\infty}}{1 - Y_{A,s}} \right)$$

transfer \times : R

$$1 + B_Y \equiv \frac{1 - Y_{A,\infty}}{1 - Y_{A,s}}$$

$$B_Y \rightarrow \frac{Y_{A,s} - Y_{A,\infty}}{1 - Y_{A,s}}$$

$$\dot{m} = 4\pi r_s \rho D_{AB} \ln(1 + B_Y)$$

$$B_Y \rightarrow 0 \quad \dot{m} \rightarrow 0$$

$$B_Y \uparrow \quad \dot{m} \uparrow$$

Droplet mass conservation:

$$\frac{d m_{\text{drop}}}{dt} = -\dot{m}$$

$$m_{\text{drop}} = \rho_{\text{liq}} V = \rho_{\text{liq}} \frac{\pi D^3}{6}$$

$$= \rho_{\text{liq}} \frac{\pi (8 r_s^3)}{6}$$

$$\frac{d \left(\frac{4}{3} \pi r_s^3 \rho_e \right)}{dt} = -\dot{m} = -4\pi r_s \rho D_{AB} \ln(1 + B_Y)$$

$$\frac{1}{3} \rho_e \frac{dr_s^3}{dt} = -r_s \rho D_{AB} \ln(1 + B_Y)$$

$$\cancel{3} r_s^2 \cancel{\rho_l} \frac{dr_s}{\cancel{3} \partial t} = -r_s \rho D_{AB} \ln(1+B_y)$$

$$\frac{dr_s}{\partial t} = \frac{-\rho}{\rho_l} \frac{D_{AB}}{r_s} \ln(1+B_y)$$

$$\frac{dD}{\partial t} = \frac{-4\rho}{\rho_l} \frac{D_{AB}}{D} \ln(1+B_y)$$

$$\frac{dD^2}{\partial t} = \frac{-8\rho}{\rho_l} D_{AB} \ln(1+B_y)$$

evaporation const. K

$$K = \frac{8\rho}{\rho_l} D_{AB} \ln(1+B_y)$$

$$\frac{\partial D^2}{\partial t} = -K$$

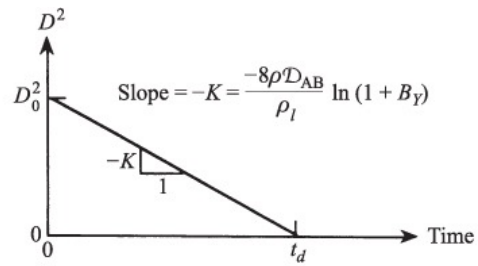
t_d = time to completely evaporate droplet

$$\int_{D_0^2}^0 \partial D^2 = \int_0^{t_d} -K$$

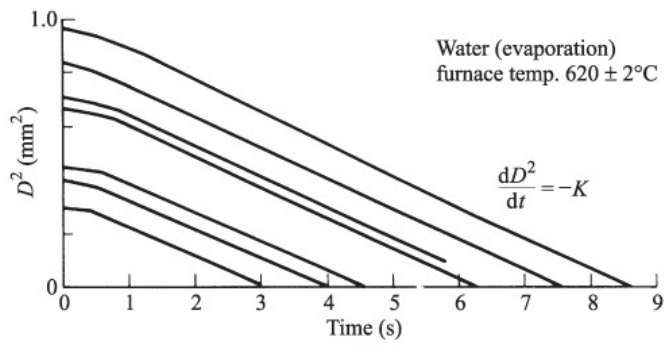
$$t_d = D_0^2 / K$$

$$\text{or } D^2(t) = D_0^2 - Kt$$

D^2 law



(a)



(b)

Figure 3.7 The D^2 law for droplet evaporation. (a) Simplified analysis. (b) Experimental data from Ref. [8] for water droplets with $T_\infty = 620^\circ\text{C}$.
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